

Unit: I- Introduction to Electric Drives

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Discussed in the Previous Class

In the previous class discussed the following topics:

- Components of Load Torque
- Classifications of Load Torque

Lecture Outcomes

Time and Energy Loss in Transient Operations

- Steady State Stability of an Electric Drive System
- Lecture remarks: Key points of today's class





Starting, braking, speed change and speed reversal are transient operations. Time and Energy Loss in Transient Operations can be evaluated by solving Eq. (6) along with motor circuit equations. T_2 , T_3 , T_4

> When T and T_{L} are constants or proportional to speed, Eq. (6) will be a first-order linear differential equation. Then it can be solved analytically.

 $T = J \frac{d\omega_{\rm m}}{dt} + T_{\rm L} + B\omega_{\rm m}$

> When T or T_L is neither constant nor proportional to speed, (6) will be a non-linear differential equation.
T and T_L
> It could then be solved numerically by the Runga-Kutta method.

(6)

T= JdWm + TLF BWm. T 77 TL 77 BWM T&TL >> BUM vert Less. T= J(dwm) + Trunie de + Trunie エール wm(T-Tr

- For any of the above mentioned transients, the final speed is an equilibrium speed.
- Theoretically, transients are over in infinite time, which is not so in practice.
- To resolve this anomaly, Time and Energy Loss in Transient Operations is considered to be over when 95% change in speed has taken place.
- For example, when speed changes from ω_{m1} to equilibrium speed ω_{me} , the time taken for the speed to change from ω_{m1} to $[\omega_{m1} + 0.95(\omega_{me} - \omega_{m1})]$ is considered to be equal to the transient time.



- Transient time and energy loss can also be computed with satisfactory accuracy using steady-state speed-torque and speed-current curves of the motor and speed-torque curve of load. $\sqrt{\frac{1}{2}}$, $\sqrt{\frac{1}{2}}$, $\sqrt{\frac{1}{2}}$, $\sqrt{\frac{1}{2}}$
- This is because the mechanical time constant of a drive is usually very large compared to the electrical time constant of a motor.
- Consequently, electrical transients die down very fast and motor operation can be considered to take place along the steady-state speed-torque and speed-current curves. From $(T = T_1 + Jd\omega_m/dt)$

$$dt = \frac{Jd\omega_{\rm m}}{T(\omega_{\rm m}) - T_l(\omega_{\rm m})} \tag{7}$$

→ where $T(\omega_m)$ and $T_1(\omega_m)$ indicate that the motor and load torques are functions of drive speed ω_m .

Time taken for drive speed to change from ω_{m1} to ω_{m2} is obtained by integrating Eq. (7) $t = J \int_{\omega_{m1}}^{\omega_{m2}} \frac{d\omega_m}{T(\omega_m) - T_l(\omega_m)} \qquad (8)$

Equation (8) can be integrated only if functions $T(\omega_m)$ and $T_1(\omega_m)$ are known and are of integral form.



- > When ω_{m2} is an equilibrium speed ω_{me} , then the reciprocal of acceleration will become infinite at ω_{me} . Consequently, time evaluated this way will be infinite.
- > Therefore, in this case transient time is computed by measuring the area between speeds ω_{m1} and $\omega_{m1} + 0.95(\omega_{m2} \omega_{m1})$.

Energy dissipated in a motor winding during a transient operation is given by $E = \int_{0}^{t} i^{2} dt$ $E = \int_{0}^{t} Ri^{2} dt$ $F = \int_{0}^{t} Ri^{2} dt$

 \succ where R is the motor winding resistance and *i* is the current flowing through it.



- Equilibrium speed of a motor-load system is obtained when motor torque equals the load torque. $T_1 = T$
- Drive will operate in steady-state at this speed, provided it is the speed of stable equilibrium.
- Concept of Steady State Stability of Drive has been developed to readily evaluate the stability of an equilibrium point from the steady-state speed-torque curves of the motor and load, thus avoiding solution of differential equations valid for the transient operation of the drive.

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- In most drives, the electrical time constant of the motor is negligible compared to its mechanical time constant.
- Therefore, during transient operation, motor can be assumed to be in electrical equilibrium implying that steady-state speed-torque curves are also applicable to the transient operation.



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- As an example let us examine the Steady State Stability of Drive of equilibrium point A in Fig. 2.9(a).
- The equilibrium point will be termed as stable when the operation will be restored to it after a small departure from it due to a disturbance in the motor or load. $\int \omega_m = \omega_m - \omega_m$
- > Let the disturbance cause a reduction of $\Delta \omega_{\rm m}$ in speed.
- At new speed, the motor torque is greater than the load torque, consequently, the motor will accelerate and operation will be restored to A. Similarly, an increase of $\Delta \omega_m$ in speed caused by a disturbance will make load torque greater than the motor torque, resulting into deceleration and restoration of operation to point A. Hence the drive is steady-state stable at point A.



Fig. 7. Point A is stable.

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- ➢ Let us now examine equilibrium point B which is obtained when the same motor drives another load.
- A decrease in speed causes the load torque to become greater than the motor torque, the drive decelerates and the operating point moves away from B.
- Similarly, when working at B an increase in speed will make motor torque greater than the load torque, which will move the operating point away from B.
- Thus, B is an unstable point of equilibrium. Readers may similarly examine the Steady State Stability of Drive of points C and D given in Figs. (9) and (10).



Fig. 10. Point D is unstable. ¹⁴

Above discussion suggests that an equilibrium point will be stable when an increase in speed causes load-torque to exceed the motor torque, i.e. when at equilibrium point following condition is satisfied: T_{i}

Inequality (2.24) can be derived by an alternative approach. Let a small perturbation in speed, $\Delta \omega_{m}$ results in ΔT and ΔT_1 perturbations in T and T_1 respectively. Then from From $(T = T_1 + Jd\omega_m/dt)$

 $\frac{dT_l}{d\omega_m} > \frac{dT}{d\omega_m} \qquad dT_L = \sigma T \qquad (10)$

Subtracting (fundamental torque equation: $(T = T_1 + Jd\omega_m/dt))$ from (11) and rearranging terms gives



For small perturbations, the speed torque curves of the motor and load can be assumed to be straight lines. Thus T = T



where $(dT/d\omega_m)$ and $(dT_l/d\omega_m)$ are respectively slopes of the steady-state speed-torque curves of motor and load at operating point under consideration. Substituting Eqs. (13) and (14) into (12) and rearranging the terms yields

$$J \frac{d\Delta\omega_{\rm m}}{dt} + \left(\frac{dT_l}{d\omega_{\rm m}} - \frac{dT}{d\omega_{\rm m}}\right) \Delta\omega_{\rm m} = 0$$
(15)

This is a first order linear differential equation. If initial deviation in speed at t = 0 be $(\Delta \omega_m)0$ then the solution of Eq. (15) will be

$$\Delta\omega_{\rm m} = (\Delta\omega_{\rm m})_0 \exp\left\{-\frac{1}{J}\left(\frac{dT_l}{d\omega_{\rm m}} - \frac{dT}{d\omega_{\rm m}}\right)t\right\}$$
(16)

An operating point will be stable when $\Delta \omega_m$ approaches zero as t approaches infinity. For this to happen the exponent in Eq. (16) must be negative.

Key Points from Today's Class

Time and Energy Loss in Transient Operations

Steady State Stability of an Electric Drive System

Key Points from Next Class

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Thank you so much for your attentions Q & A